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MANUFACTURING METHODS AND TECHNOLOGY (MM AND T) MEASURE FOR FAB--ETC(U)  
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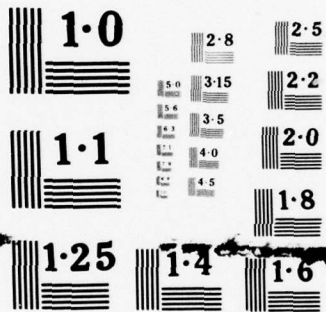
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THIRD QUARTERLY PROGRESS REPORT

MANUFACTURING METHODS AND TECHNOLOGY ( MM & T )  
MEASURE FOR FABRICATION OF THIN FILM ALUMINUM  
OXIDE (  $Al_2O_3$  ) ION BARRIER 18MM MICROCHANNEL  
PLATES

( TITLE UNCLASSIFIED )

1 JANUARY 1977 TO 31 MARCH 1977  
CONTRACT NO. DAAB07 - 76 - C - 0043

U. S. ARMY ELECTRONICS COMMAND  
PRODUCTION DIVISION  
PRODUCTION INTEGRATION BRANCH  
FORT MONMOUTH, NEW JERSEY 07703

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MMTE FOR  $Al_2O_3$  ION

BARRIER MCPs

THIRD QUARTERLY REPORT

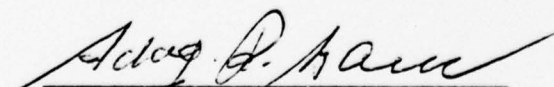
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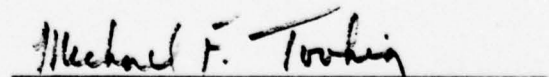
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## ABSTRACT (U)

- (U) Effort during the third quarter of the contract was concentrated on fabrication and testing of the second submission of 10 engineering samples. In addition, tasks continued during the report period include: 1) achievement of uniform fire polishing of entire MCP input surface by using a mesh heater structure, 2) improved MCP surface quality by optimizing prepoly condition of MCP's and 3) employment of thicker lacquer films to improve  $Al_2O_3$  quality.
- (U) The new Varian evaporator was completed and used to perform all  $Al_2O_3$  evaporations. To achieve better thickness control, a dual shutter system was employed. Several flood gun designs were tested in the present engineering demountable test head to achieve higher electron density for improved viewing of  $Al_2O_3$  film defects.
- (U) Several MCP's were coated with very thick  $Al_2O_3$  films to study  $Al_2O_3$  film defects. The bakeable demountable test system was completely assembled and is now undergoing heat and pressure tests.



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## 1.0 INTRODUCTION (U)

(U) The purchase description DAAB07-76-R-0035 calls for a manufacturing methods and technology measure (MMTE) for "Aluminum Oxide"  $Al_2O_3$  which meet the MCP 003 requirements. The objective of this program is to establish a production capability for the purpose of meeting estimated military needs for a period of two years after completion of the contract, and to establish a base in plans which may be used to meet expanded requirements. The MMTE will include all work under Paragraphs 3.1 and 3.2 of ECIPPR No. 15 necessary to establish capability to manufacture aluminum oxide ion barrier microchannel plates on a pilot line basis including fabrication of engineering samples and confirmatory samples as specified in the contract. Included in this program as part of the engineering phase are the investigation of improvements in surface conditions and cleanliness for MCP's to be filmed, salvage of  $Al_2O_3$  ion barrier MCP's, filming process control, the achievement of optimum performance characteristics for ion barrier MCP's and the design and fabrication of specialized test equipment.

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## 2.0 TECHNICAL DISCUSSION (U)

### 2.1 $\text{Al}_2\text{O}_3$ Ion Barrier Formation (U)

#### 2.1.1 MCP Surface Cleaning (U)

(U) In addition to closer inspection and particle picking of MCP's prior to filming, edge grinding of the polished MCP has been introduced as part of the cleaning process. During the standard polishing process, cerium oxide particles are embedded into the beveled edge of the MCP as it shifts position in the polishing holder during the polishing operation. To remove embedded particles, the polished MCP is edge ground which is accomplished by loading the MCP into a vacuum chuck, rotating the plate and grinding the exposed edge with a honing tool. Edge grinding has resulted in much cleaner plates and has reduced the number of type A and B holes in the  $\text{Al}_2\text{O}_3$  film.

#### 2.1.2 Improved Lacquering Techniques (U)

(U) Investigations of improved lacquering techniques have included use of an overflow lacquering tank for achieving a cleaner water surface, control of lacquer thickness, and investigation of lacquer set up and drying time.

During the last portion of this quarter, attempts were made to lacquer funneled plates on another program. In filming funneled plates, the lacquer is only supported by very thin edges of the MCP matrix glass. Using the standard lacquering process, lacquer films sagged and ruptured when stretched across the funneled active area

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of the MCP. Sagging and rupturing was eliminated by employing a thicker lacquer film. Thicker lacquer films can be produced by slightly increasing the temperature of the water bath. Warmer water speeds up the drying process of the lacquer and therefore, limits spreading of the lacquer on the water surface. This technique was successfully used to lacquer and film funneled MCP's.

The same technique was then applied to standard plates and test results have shown that thicker films effectively reduce the number of type A holes in the finished plate.

## 2.1.3 $\text{Al}_2\text{O}_3$ Ion Barrier Evaporation (U)

### 2.1.3.1 Vacuum Baking of $\text{Al}_2\text{O}_3$ Films (U)

- (U) Prior to completion of the second submission of engineering samples, it was found that vacuum baking of  $\text{Al}_2\text{O}_3$  ion barrier MCP's resulted in thinning of the  $\text{Al}_2\text{O}_3$  film and hence in a reduction in dead voltage and gain change between 800 and 1000 volts input landing energies. The same decrease in dead voltage was measured in tubes after processing in a parallel tube program.
- (U) To confirm these results, several ion barrier plates were vacuum baked at  $375^\circ\text{C}$  for 8 hours. The test results are shown in Table I.
- (U) These test results show that vacuum baking of ion barrier MCP's reduced the thickness of  $\text{Al}_2\text{O}_3$  ion barrier films. The average reduction in gain change and in dead voltage was 40%. To compensate for the reduction in film thickness during vacuum bake, the thickness of the  $\text{Al}_2\text{O}_3$  film

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Table I (U)

<u>Plate #</u>	<u>Thickness</u>	<u>Prior to Bake Gain Change/ Dead Voltage</u>	<u>After Bake Gain Change/ Dead Voltage</u>
538-11	45 Å	8% / 80 Vdc	5%/60 Vdc
538-09	47 Å	7.5% / 85 Vdc	4%/30 Vdc
538-19	42 Å	7.7% 80 Vdc	5%/50 Vdc
538-16	42 Å	6% / 80 Vdc	4%/30 Vdc
538-07	42 Å	5% / 45 Vdc	0% / 0 Vdc

was increased. Additional MCP's were prepared with a 63 Å thick  $Al_2O_3$  film. The test results, before and after vacuum bake, are shown in Table II.

Table II (U)

<u>Plate #</u>	<u>Thickness</u>	<u>Prior to Bake Gain Change/ Dead Voltage</u>	<u>After Bake Gain Change/ Dead Voltage</u>
317-27	63 Å	15% / 260 Vdc	5.3%/190 Vdc
538-26	63 Å	16% / 270 Vdc	11.3%/170 Vdc
317-32	63 Å	18% / 250 Vdc	16% / 210 Vdc
317-30	63 Å	16% / 260 Vdc	15% / 180 Vdc
317-24	63 Å	15% / 230 Vdc	13% / 180 Vdc
317-45	63 Å	15.5% / 240 Vdc	15% / 180 Vdc
538-21	63 Å	15% / 225 Vdc	13.5%/165 Vdc

(U) In contrast to the results shown in Table I, the second experiment yielded a drop in gain change and dead voltage of only 25%.

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(U) In addition to the above tests, three MCP's from Table I were rebaked at 375°C for 8 hours. The test results are shown in Table III which show that the second vacuum bake does not affect the gain change and dead voltage appreciably.

Table III (U)

<u>Plate#</u>	<u>Thickness</u>	<u>Prior Bake Gain Change/ Dead Voltage</u>	<u>After Bake Gain Change/ Dead Voltage</u>	<u>After 2nd Bake Gain Change/ Dead Voltage</u>
538-19	42 Å	7.7%/80 Vdc	5%/50 Vdc	4%/ 10 Vdc
538-09	47 Å	7.5%/85 Vdc	4%/30 Vdc	5.8%/ 45 Vdc
538-11	45 Å	8%/ 80 Vdc	5%/60 Vdc	5%/ 50 Vdc

(U) Based on the results shown in Table II additional plates were evaporated with a 55 Å thick  $Al_2O_3$  film. As shown in Table IV, a gain change of slightly less than 10% and a dead voltage of 150 Vdc were achieved after vacuum bake.

Table IV (U)

<u>Plate #</u>	<u>Thickness</u>	<u>Before Bake Gain Change/ Dead Voltage</u>	<u>After Bake Gain Change/ Dead Voltage</u>
542-32	55 Å	10%/200 Vdc	7%/140 Vdc
542-33	55 Å	11%/185 Vdc	9%/140 Vdc

(U) These experiments have shown that the required maximum gain change of 10% and maximum dead voltage of 150V can be met with a 55 Å thick  $Al_2O_3$  film after a vacuum bake at 375°C for 8 hours.

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2.1.3.2  $\text{Al}_2\text{O}_3$  Film Evaporation With Varian Evaporator. (U)

- (U) During this report period, the new oil free Varian Evaporator was made operational. Experiments were performed to establish evaporation conditions and to achieve  $\text{Al}_2\text{O}_3$  film characteristics with respect to gain change and dead voltage identical to those achieved with  $\text{Al}_2\text{O}_3$  films prepared with the Veeco evaporator. Identical film characteristics were achieved with a deposited film thickness of 40-42 $\text{\AA}$  as compared to 55 $\text{\AA}$  with the Veeco evaporator. The reduced film thickness may be attributed to the lower vacuum pressure during evaporation. The new evaporator maintains a vacuum pressure of  $5 \times 10^{-6}$  Torr during evaporation as compared to an average of  $5 \times 10^{-5}$  Torr with the Veeco evaporator.
- (U) To establish accurate rate control and deposition, a dual shutter system was designed and installed in the Varian evaporator. The dual system consists of a scissors shutter which is located directly below the MCP substrate holder and an evaporant outgassing shutter which is located directly above the E-gun hearth. The "scissors" shutter consists of two semi-circular plates and a circular cutout in the closed position which is in line with the sensor head and the evaporant source. After initial outgassing of the  $\text{Al}_2\text{O}_3$  evaporant in the evaporation boat, the outgassing shutter is swung open to expose the thickness monitor to the vapor stream. The evaporation rate is then adjusted to 1 to 2 $\text{\AA}$  per second. During this adjustment period, the scissors shutter is in the closed position to protect the MCP's from  $\text{Al}_2\text{O}_3$  vapors. The outgassing shutter is then moved over the evaporation boat

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to re-zero the thickness monitor. The scissors shutter is then opened and the outgassing shutter is then quickly swung open. After 40Å of  $\text{Al}_2\text{O}_3$  have been evaporated, the outgassing shutter and scissors shutter are closed again. This dual shuttering technique has greatly improved  $\text{Al}_2\text{O}_3$  deposition control.  $\text{Al}_2\text{O}_3$  films of desired thickness can now be produced on a reproducible basis.

## 2.2 MCP Surface Quality Improvement (U)

### 2.2.1 Grinding and Polishing (U)

(U) To improve the pre-polish condition of the MCP surface, twenty-two MCP's were ground with a mixture of 5 micron particle grinding compound and Cerite polishing compound mixed in a ratio of 4:1. MCP surfaces were then polished by utilizing the standard production polishing process. After removal of the core glass in 10% solution of HCl, the surface of the MCP did not reveal any scratches which normally appear at this stage. A photograph of the surface of a standard MCP is shown in Figure #1. Surface scratches can be seen on the matrix of the MCP. As a comparison, Figure #2 shows the etched surface of an MCP which has been prepared with the improved pre-polish technique. No surface scratches can be detected. To confirm these results, a second group of MCP's will be prepared during the 4th quarter with the improved pre-polish technique.

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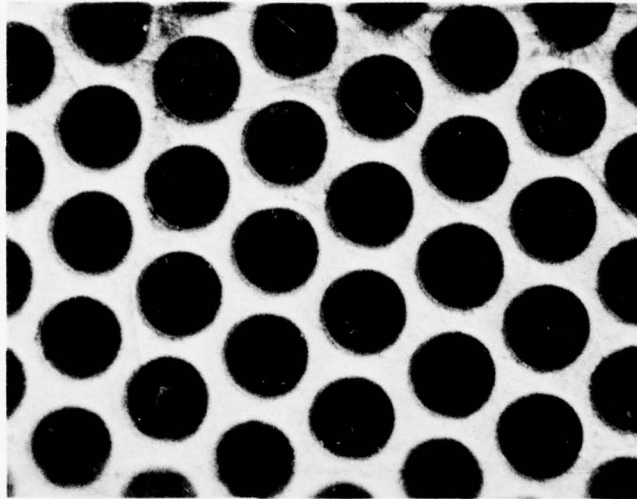


FIGURE #1 (U) Normal Production MCP Surface  
After Chemical Etching and Cleaning.

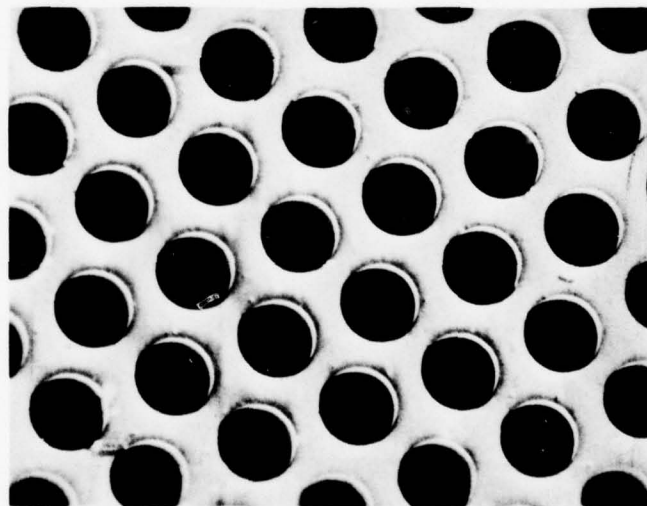


FIGURE #2 (U) Improved "Pre-Polish" Condition  
MCP Surface After Chemical  
Etching and Cleaning.

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## 2.2.2 Fire Polishing (U)

- (U) Fire polishing experiments were continued utilizing a square tantalum heating mesh. These experiments have produced uniform fire polishing action across the entire MCP surface.
- (U) Fire polishing is accomplished in the following manner. The MCP is located in vacuum with a heat source in close proximity to the input side. The heat source is activated which then raises the glass surface to just below the melting temperature. To achieve a smooth and uniform fire polished surface, the temperature is peaked to the melting point and then reduced to room temperature.
- (U) This technique has resulted in one uniformly fire polished MCP. However, subsequent experiments have clearly demonstrated that fire polishing conditions are extremely difficult to reproduce. The decision was then made to discontinue this technique in favor of the more successful pre-polish technique.

## 2.3 Testing of $\text{Al}_2\text{O}_3$ Ion Barrier Films (U)

### 2.3.1 Tube Construction (U)

- (U) In preparation for the confirmatory sample phase of the contract, two test tubes were constructed with  $\text{Al}_2\text{O}_3$  ion barrier MCP's. Both tubes were built using production sub assemblies and utilizing standard Generation II production facilities. Special handling of filmed MCP's

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was introduced to insure that the  $\text{Al}_2\text{O}_3$  film was not picked or blown clean during assembly and exhaust loading operations. After both tubes were completed, testing at 5 volts landing energy revealed many more "hole" defects in the  $\text{Al}_2\text{O}_3$  film than had been detected by the demountable test head using UV excitation of an aluminized quartz cathode as the emission source. The appearance of more holes in the  $\text{Al}_2\text{O}_3$  film of the finished tubes may be related to tube processing techniques or more holes may be detectable with the higher electron density from the photocathode. To determine if more holes can be detected with higher electron density, the demountable test head was equipped with a flood gun capable of higher electron emission than the presently employed UV excited aluminized quartz cathode.

- (U) Both tubes were assembled and exhausted without difficulty. For simplicity, the tubes were assembled using the single seal method and the MCP was outgassed with a standard GEN II flood gun.

## 2.3.2 Flood Gun MCP Testing (U)

- (U) Our present engineering demountable test station is equipped with two test heads. One of the test heads was modified for flood gun viewing of  $\text{Al}_2\text{O}_3$  filmed MCP's whereas the second test head is equipped with a UV excitation source. A standard GEN II MCP outgassing gun was modified to achieve flood gun electron excitation of the  $\text{Al}_2\text{O}_3$  ion barrier MCP. Despite employment of a mesh



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between the flood gun and the test MCP, the uniformity of the flood beam was poor. However, sufficient testing was performed to determine that the flood gun viewing system is capable of detecting all holes which are detectable with the UV excited test head, and in addition, the flood gun viewing system is capable of resolving smaller holes in the film than could be detected with the UV excited test head.

## 2.3.3 Defect Study Using Thick $\text{Al}_2\text{O}_3$ Films. (U)

- (U) In an effort to correlate film defects which are detectable by electron viewing with film defects which are visually detectable under the Leitz microscope, MCP's were prepared with thick  $\text{Al}_2\text{O}_3$  films. One MCP was evaporated with 500Å of  $\text{Al}_2\text{O}_3$ . The second sample was evaporated with 250Å of  $\text{Al}_2\text{O}_3$ . Thicker films facilitate visual detection of very small (2-3 micron) defects in the  $\text{Al}_2\text{O}_3$  film.
- (U) Figure #3 shows a plate when viewed with the flood gun. This MCP was originally rejected in the UV test head for an excessive number of type A and B holes. After rejection, it was re-evaporated with 500 additional Å of  $\text{Al}_2\text{O}_3$  for defect studies. In Figure #4, the large bright spot appearing near the edge of the MCP at the bottom of the photograph was located visually and photographed using the Leitz microscope. This defect is illustrated in Figure #4, and apparently is a break in the lacquer film exposing an area of at least six single channels. Close examination of the defect revealed a raised edge around the periphery of the defect

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FIGURE #3 (U) Photograph of Reject  $\text{Al}_2\text{O}_3$ .  
Filmed MCP as Viewed with the  
Flood Gun Test Head.

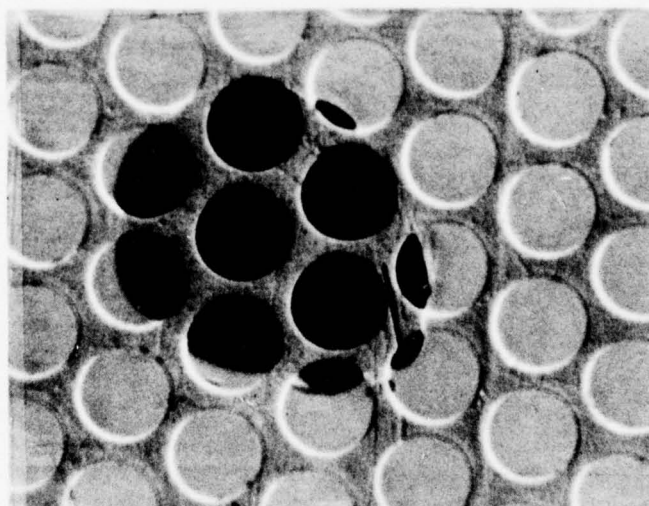


FIGURE #4 (U) Photograph of Large Hole in the  
Lacquer Film Probably Present  
Prior to  $\text{Al}_2\text{O}_3$  Evaporation.

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which consists of the rolled lip of the lacquer film. Other defects in thick  $\text{Al}_2\text{O}_3$  film MCP's are illustrated in Figures 5, 6, and 7. Additional tests will be required to determine and isolate causes for film defects.

## 2.4 Bakeable and Demountable Vacuum Test System (U)

- (U) The demountable system was completely assembled at the end of the third quarter. A photograph of the assembled system is shown in Figure #8. The delayed SCR heat controller has since been received. The entire system is presently undergoing heat and pressure tests.
- (U) The entire vacuum system has been leak checked. A nude UHV gauge has been installed in the chamber to permit pressure testing of the demountable chamber during heat cycling. A photograph of the demountable chamber is shown in Figure #9.
- (U) After all leak checking at room temperature and at  $375^\circ\text{C}$  has been completed, the internal fixturing will be installed. The internal fixturing consists of 1) a fixed circular plate containing either aluminized cathodes or openings for flood gun electrons arranged in a circle, 2) a rotatable plate containing six ceramic nests arranged in a circle and 3) a support stand which locates the six ceramic nests directly below viewing ports which are situated on top of the chamber.



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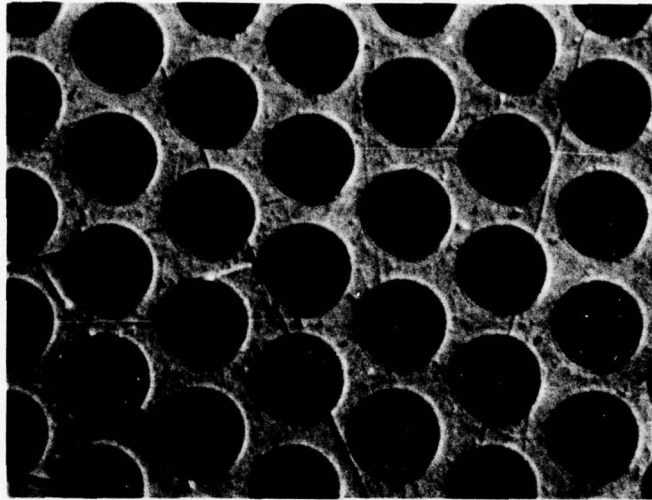


FIGURE #5 (U) Completed MCP With  $Al_2O_3$  Film  
Illustrating a Small 3-4 Micron Hole  
in Lacquer Film. Hole May Be Caused  
by  $Al_2O_3$  "Pop-Up" During Evaporation.  
Appears as Defect in Demountable.

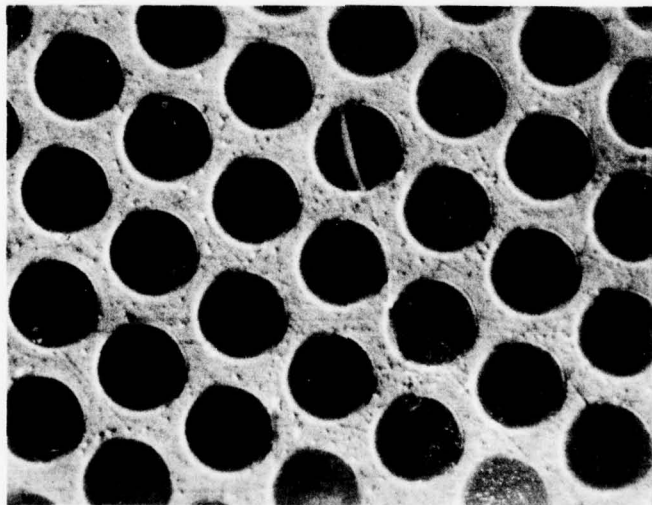


FIGURE #6 (U) Completed MCP With  $Al_2O_3$  Film  
Illustrating Splits in Lacquer  
Film. May Be Weakness in Lacquer.  
Appears as Defect in Demountable.

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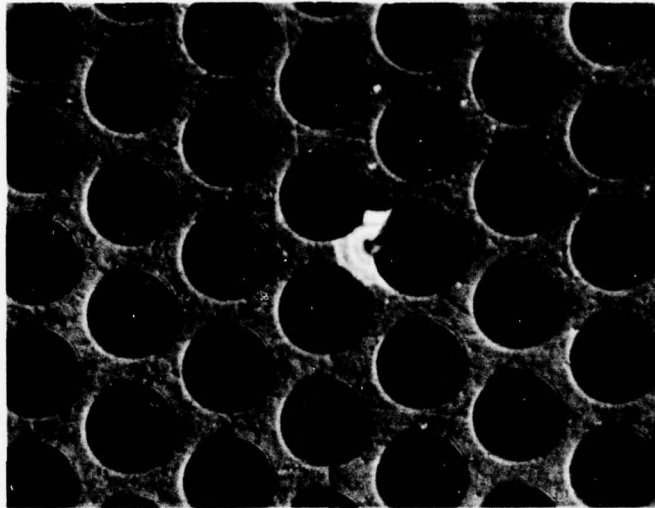


FIGURE #7 (U) Dust Particles Under  $\text{Al}_2\text{O}_3$   
Film. Appears as Defect  
in Demountable.

**UNCLASSIFIED**

**UNCLASSIFIED**

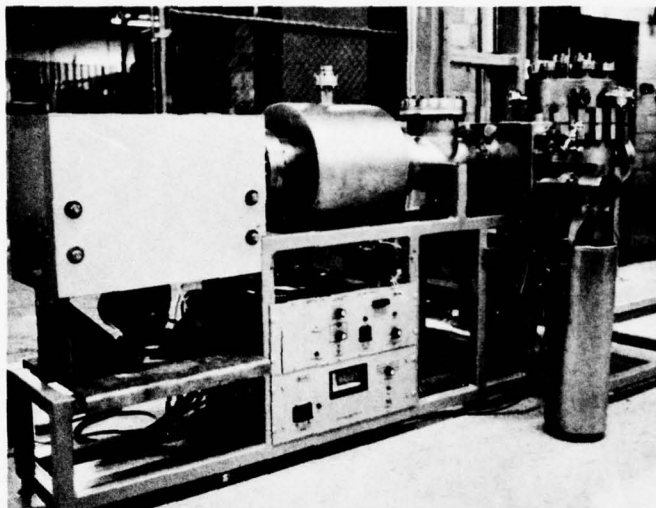


FIGURE #8 (U) Photograph of Test Chamber and Pumping System.

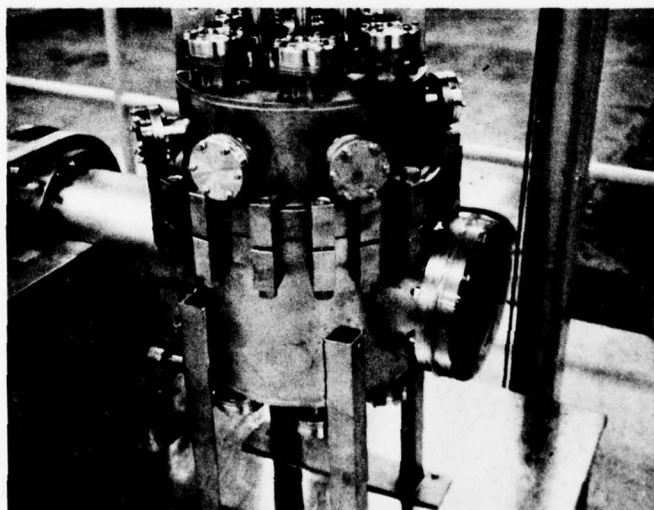


FIGURE #9 (U) Bakeable Demountable Test Chamber.

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(U) Each ceramic nest contains a test MCP and a phosphor faceplate which can be rotated over any of the fixed outgas or test positions. This arrangement permits each MCP to be electron scrubbed with a flood gun and tested with either a flood gun or UV excited aluminized cathode for electrical characteristics and ion barrier film quality.

(U) Electrical connections to the MCP input and output, aluminized cathodes and flood gun electrodes are made through the bottom section of the chamber. High voltage connections to the six phosphor plates are already mounted in the top portion of the chamber.

## 2.5 Preparation and Delivery of Second Submission of 10 Engineering Samples (U)

(U) The second submission of ten (10) engineering samples was submitted on February 28, 1977. Category II requirements for these samples include nine non-bake requirements and two requirements after bake. Each MCP after it had been tested and met the nine non-bake requirements was individually loaded into a tube body and baked for 8 hours at 375°C. The vacuum bake requirements for category II tests were also met. The MCP's were then retested in the demountable test head for correlation of test results. Test data for the 10 engineering samples are given in Table V. Detailed test data for each MCP are presented in Figures 10 through 19.

(U) The engineering demountable test head and the new bakeable demountable system need to be equipped with

Table V,  
2ND GROUP ENGINEERING SAMPLES  
TEST SUMMARY SHEET  
MCP-003  
3-4-77

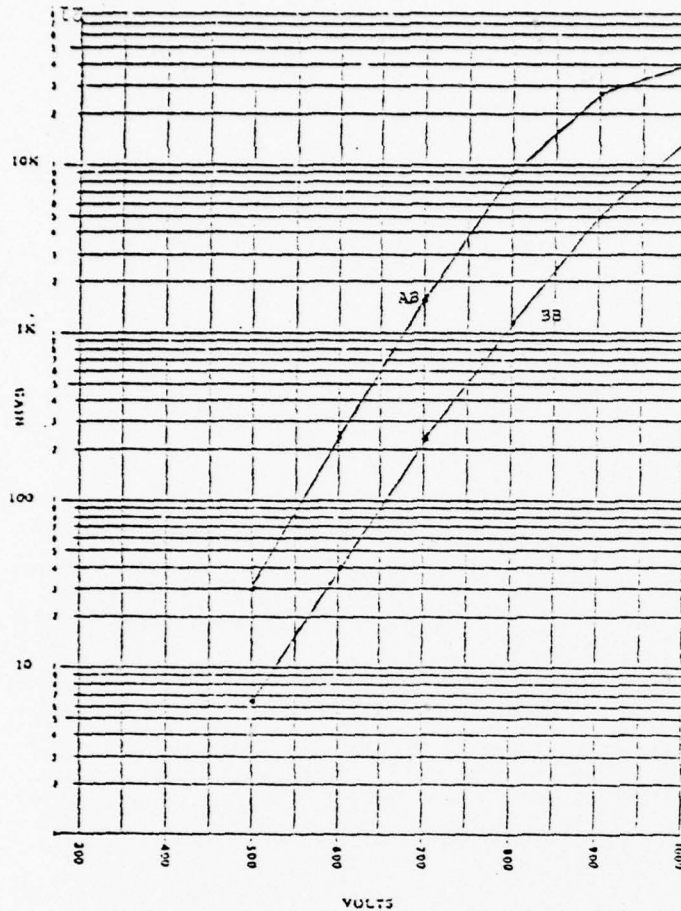
REQUIREMENT	3.3.1.1	3.3.1.2	3.3.1.3	3.3.1.4	3.3.1.5.1	3.3.1.5.2	3.3.1.5.3	3.3.1.6.2	3.3.2	3.3.1.7.1	3.3.1.7.3
TEST	4.5.2.1	4.5.2.2	4.5.2.3	4.5.2.4	4.5.2.5.1	4.5.2.5.2	4.5.2.5.3	4.5.2.6.2	4.5.2.1.0	4.5.2.2	4.5.2.4
TITLE	PENE- TRATION VOLTAGE	GAIN	DARK CURRENT	RESIS- TANCE ( $\times 10^8$ OHMS)	TYPE A HOLES	TYPE B HOLES	OTHER HOLE DEFECTS	HALATION, HOT SPOTS & FIELD EMISSION	MICRO- SCOPIC WHISKER GROWTH	GAIN	RESIS- TANCE ( $\times 10^8$ OHMS)
SPECIFICATION MCP #	10% MAX	4000 MIN	8.5 $\times 10^{-16}$ MAX	1-5 $\times 10^8$ $\Omega$	30 MAX	5 MAX	0	NONE	NONE	3000 MIN AT 900V	1-6 $\times 10^8$ $\Omega$
542-30	8.0	5000	0	3.9	2	2	0	NONE	NONE	28000	3.6
542-33	9.0	8000	0	5.0	3	2	0	NONE	NONE	23666	4.7
542-32	7.0	5000	0	5.0	5	1	0	NONE	NONE	23666	3.0
542-26	10.0	5333	0	3.1	12	1	0	NONE	NONE	19000	3.0
464-T1	7.0	6333	0	4.8	5	1	0	NONE	NONE	14333	4.4
464-T6	7.0	5333	0	3.2	6	1	0	NONE	NONE	23666	2.9
464-T5	8.0	5666	0	3.7	25	1	0	NONE	NONE	24660	3.5
542-19	9.0	7575	0	3.5	15	0	0	NONE	NONE	17270	3.4
542-29	10.0	6333	0	4.0	10	1	0	NONE	NONE	21666	3.8
508-20	8.0	8900	0	5.0	3	2	0	NONE	NONE	19330	4.9

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MCP S/N 542-30  
 VENDOR ITT  
 DATE TESTED 3-2-77  
 DIA. 0.975 inches  
 THICKNESS 21.6 mils

CONDUCTIVITY: B. | A. B. | T. B.  
 @ 500V 1.28 | 1.25 | 1.1  $\mu$  amps  
 @ 1000V 2.58 | 2.78 | 2.35  $\mu$  amps  
 INPUT:  $1.5 \times 10^{-12}$  AMPS/CM<sup>2</sup>

MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	2.0 exp- 10	6.6	
600	1.2 exp- 9	40	
700	7.0 exp- 9	232	
800	3.7 exp- 8	1232	
900	1.5 exp- 7	5000	
1000	4.7 exp- 7	15660	0

BEFORE  
 LAKE  
 800 VEK

MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	9.0 exp- 10	30	
600	8.0 exp- 9	266	
700	5.3 exp- 8	1760	
800	2.75 exp- 7	9160	
900	8.4 exp- 7	28000	
1000	1.2 exp- 6	40000	0

AFTER  
 LAKE  
 800 VEK

MCP

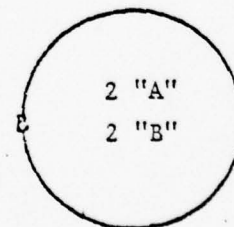
VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	3.7 exp- 11	7.0	
600	3.3 exp- 10	63	
700	2.2 exp- 9	420	
800	1.1 exp- 8	2100	
900	4.4 exp- 8	5410	
1000	1.4 exp- 7	20700	0

TEST  
 BATCH  
 800 VEK

900 VOLTS MCP  
 INPUT PENETRATION (Vi) AL<sub>2</sub>O<sub>3</sub>

VOLTS	OUTPUT CURRENT	GAIN
100E <sub>k</sub>	4.2 X10 <sup>-9</sup>	
200	8.0 X10 <sup>-9</sup>	
300	1.45 X10 <sup>-8</sup>	
400	2.1 X10 <sup>-8</sup>	
500	2.9 X10 <sup>-8</sup>	
600	3.55 X10 <sup>-8</sup>	
700	4.1 X10 <sup>-8</sup>	
800	4.45 X10 <sup>-8</sup>	
900	4.7 X10 <sup>-8</sup>	
1000	4.8 X10 <sup>-8</sup>	

3%

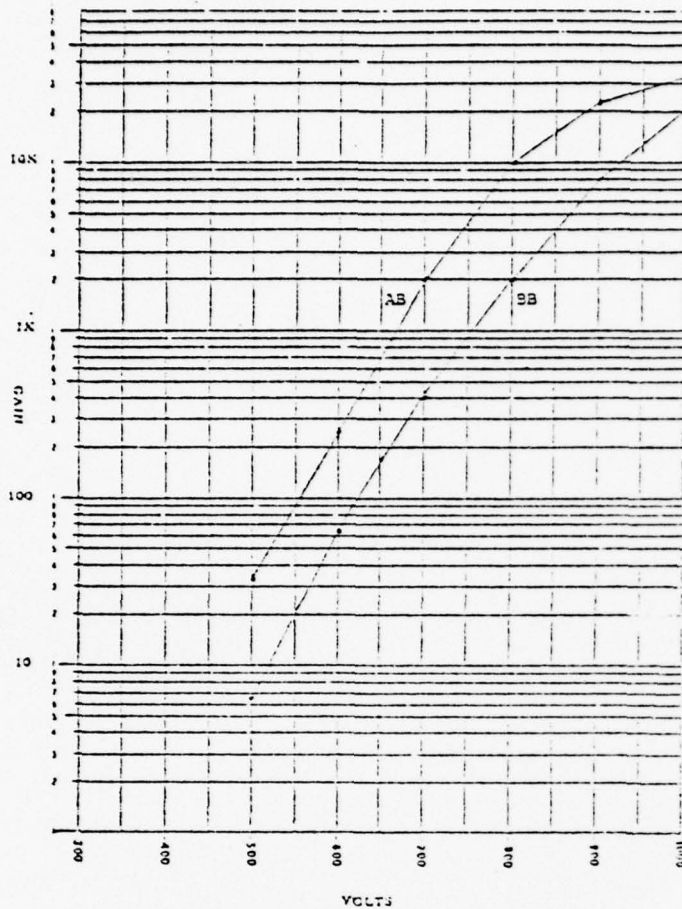


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Figure 10. TEST DATA SHEET  
 MCP #542-30

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900 VOLTS MCP  
INPUT PENETRATION (Vi)  $Al_2O_3$

VOLTS	OUTPUT CURRENT	GAIN
100 $E_k$	$2.7 \times 10^{-9}$	
200	$5.2 \times 10^{-9}$	
300	$9.1 \times 10^{-9}$	
400	$1.5 \times 10^{-8}$	
500	$2.1 \times 10^{-8}$	
600	$2.5 \times 10^{-8}$	
700	$3.0 \times 10^{-8}$	
800	$3.2 \times 10^{-8}$	
900	$3.4 \times 10^{-8}$	
1000	$3.5 \times 10^{-8}$	

92

MCP S/N 542-33  
VENDOR 11T  
DATE TESTED 3-1-77  
DIA. 0.975 inches  
THICKNESS 21.0 mils

CONDUCTIVITY:  $P.B.$   $A.P.$   $F.B.$   
(@ 500V) 0.9 0.9 0.9  $\mu$  amp  
(@ 1000V) 2.0 2.05 2.0  $\mu$  amp  
INPUT:  $1.5 \times 10^{-12}$  AMPS/ $CM^2$

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	$2.0 \times 10^{-10}$	6.6	
600	$1.2 \times 10^{-9}$	63	
700	$1.2 \times 10^{-8}$	400	
800	$6.0 \times 10^{-8}$	2000	
900	$2.4 \times 10^{-7}$	8000	
1000	$6.1 \times 10^{-7}$	20333	0

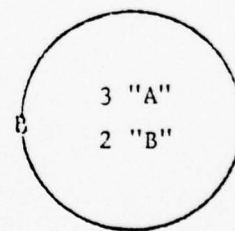
EXPON  
FAIR  
800 VEX

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	$1.0 \times 10^{-9}$	33	
600	$8.0 \times 10^{-9}$	266	
700	$6.0 \times 10^{-8}$	2000	
800	$1.0 \times 10^{-7}$	10000	
900	$7.0 \times 10^{-7}$	23333	
1000	$1.0 \times 10^{-6}$	33333	0

AFTER  
FAIR  
800 VEX

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	$2.8 \times 10^{-11}$	5.3	
600	$2.4 \times 10^{-10}$	45	
700	$1.5 \times 10^{-9}$	286	
800	$7.6 \times 10^{-9}$	1453	
900	$3.2 \times 10^{-8}$	6118	
1000	$1.1 \times 10^{-7}$	21033	0

TEST  
FAIR  
800 VEX



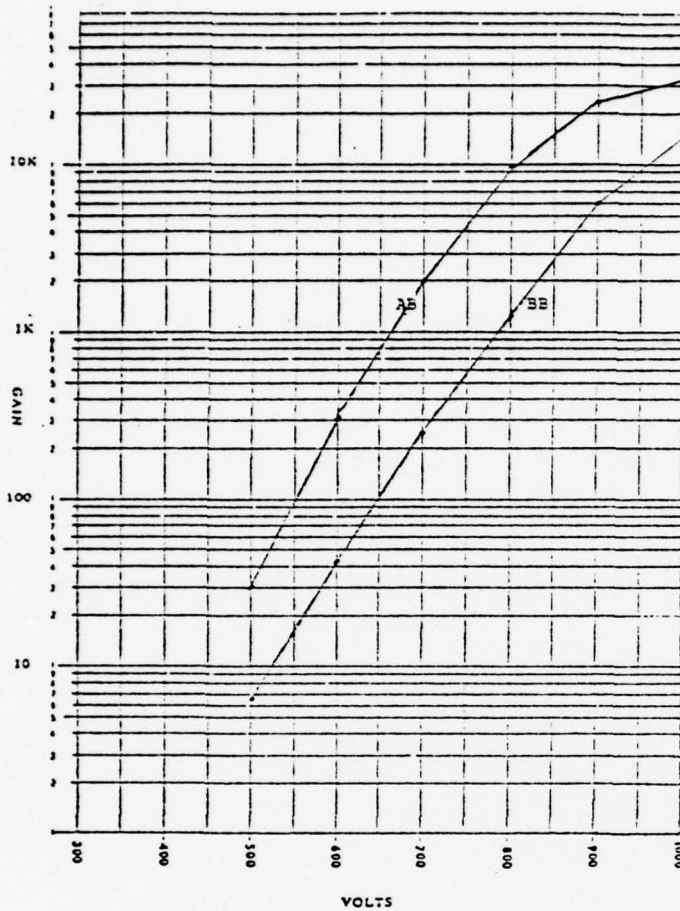
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Figure 11. TEST DATA SHEET  
MCP #542-33

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# UNCLASSIFIED



900 VOLTS MCP  
INPUT PENETRATION (Vi)  $Al_2O_3$

VOLTS	OUTPUT CURRENT	GAIN
100 $E_k$	$2.8 \times 10^{-9}$	
200	$5.3 \times 10^{-9}$	
300	$9.3 \times 10^{-9}$	
400	$1.4 \times 10^{-8}$	
500	$2.0 \times 10^{-8}$	
600	$2.4 \times 10^{-8}$	
700	$2.7 \times 10^{-8}$	
800	$2.9 \times 10^{-8}$	
900	$3.0 \times 10^{-8}$	
1000	$3.1 \times 10^{-8}$	

7%

MCP S/N 542-32  
VENDOR ITT  
DATE TESTED 2-25-77  
DIA. 0.975 inches  
THICKNESS 21.6 mils

CONDUCTIVITY: B.B. | A.B. | T.B.  
@ 500V 0.93 | 1.0 | 0.9  $\mu$  amps

@ 1000V 2.0 | 2.15 | 2.0  $\mu$  amps

INPUT:  $1.5 \times 10^{-12}$  AMPS/CM<sup>2</sup>

## MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	$2.0 \times 10^{-10}$	6.6	
600	$1.3 \times 10^{-9}$	43	
700	$8.0 \times 10^{-9}$	266	
800	$3.9 \times 10^{-8}$	1300	
900	$1.5 \times 10^{-7}$	5000	
1000	$4.4 \times 10^{-7}$	14666	0

LEFORE  
FAKE  
800 VEK

## MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	$9.0 \times 10^{-10}$	30	
600	$9.5 \times 10^{-9}$	316	
700	$6.0 \times 10^{-8}$	2000	
800	$2.9 \times 10^{-7}$	9666	
900	$7.1 \times 10^{-7}$	23666	
1000	$1.0 \times 10^{-6}$	33333	0

AFTER  
FAKE  
800 VEK

## MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	$2.6 \times 10^{-11}$	5.0	
600	$2.3 \times 10^{-10}$	44	
700	$1.5 \times 10^{-9}$	286	
800	$7.1 \times 10^{-9}$	1357	
900	$3.0 \times 10^{-8}$	5730	
1000	$1.0 \times 10^{-7}$	19100	0

TEST  
BENCH  
800 VEK

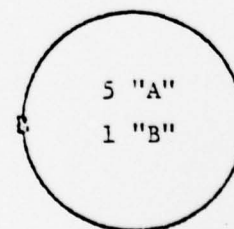
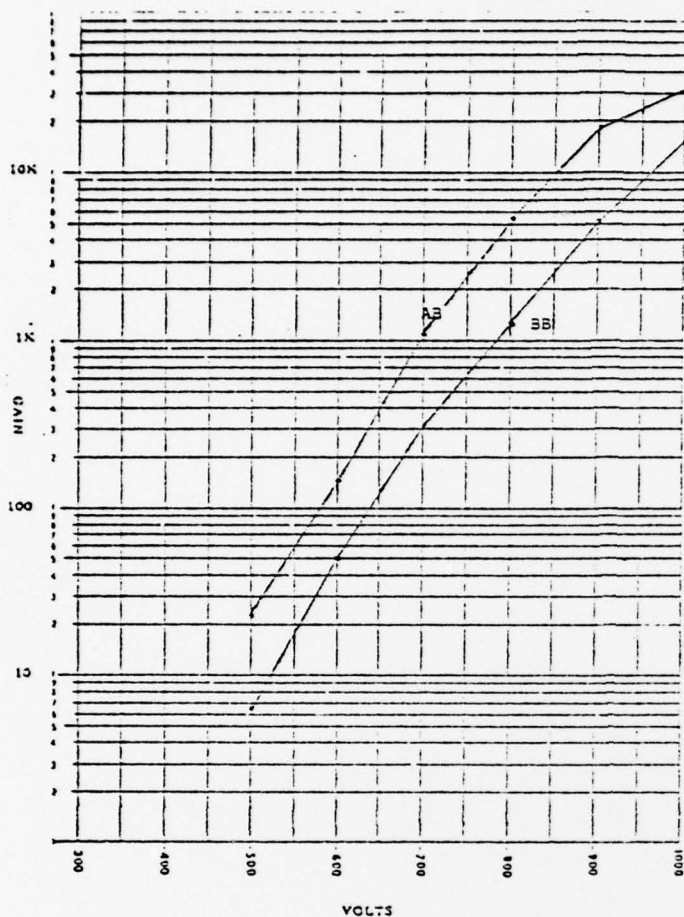


Figure 12. TEST DATA SHEET  
MCP #542-32

# UNCLASSIFIED



900 VOLTS MCP  
INPUT PENETRATION (Vi)  $Al_2O_3$

VOLTS	OUTPUT CURRENT	GAIN
100 $E_k$	$2.8 \times 10^{-9}$	
200	$5.1 \times 10^{-9}$	
300	$8.7 \times 10^{-9}$	
400	$1.4 \times 10^{-8}$	
500	$2.0 \times 10^{-8}$	
600	$2.5 \times 10^{-8}$	
700	$2.9 \times 10^{-8}$	
800	$3.15 \times 10^{-8}$	
900	$3.33 \times 10^{-8}$	
1000	$3.50 \times 10^{-8}$	

10%

MCP S/N 542-26  
VENDOR ITT  
DATE TESTED 2-23-77  
DIA. 0.975 inches  
THICKNESS 21.6 mils

CONDUCTIVITY: B. | A.B. | T.B.  
@ 500V 1.5 | 1.55 | 1.3  $\mu$  amps  
@ 1000V 3.2 | 3.3 | 2.8  $\mu$  amps  
INPUT:  $1.5 \times 10^{-12}$  AMPS/CM<sup>2</sup>

MCP	VOLTS	OUTPUT CURRENT	GAIN	BKGD.
	500	2.0 exp- 10	6.6	
	600	1.5 exp- 9	50	
	700	9.3 exp- 9	310	
	800	4.1 exp- 8	1366	
	900	1.6 exp- 7	5333	
	1000	5.1 exp- 7	17000	0

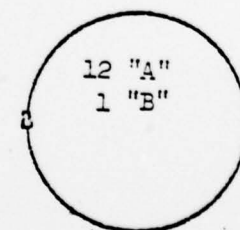
BEFORE  
BAKE  
800 VEK

MCP	VOLTS	OUTPUT CURRENT	GAIN	BKGD.
	500	7.0 exp- 10	23	
	600	4.8 exp- 9	160	
	700	3.3 exp- 8	1100	
	800	1.65 exp- 7	5500	
	900	5.7 exp- 7	19000	
	1000	9.5 exp- 7	31666	0

AFTER  
BAKE  
800 VEK

MCP	VOLTS	OUTPUT CURRENT	GAIN	BKGD.
	500	1.1 exp- 10	21	
	600	3.3 exp- 10	63	
	700	1.8 exp- 9	344	
	800	8.1 exp- 9	1550	
	900	3.2 exp- 8	6110	
	1000	9.0 exp- 8	17200	0

TEST  
BENCH  
800 VEK

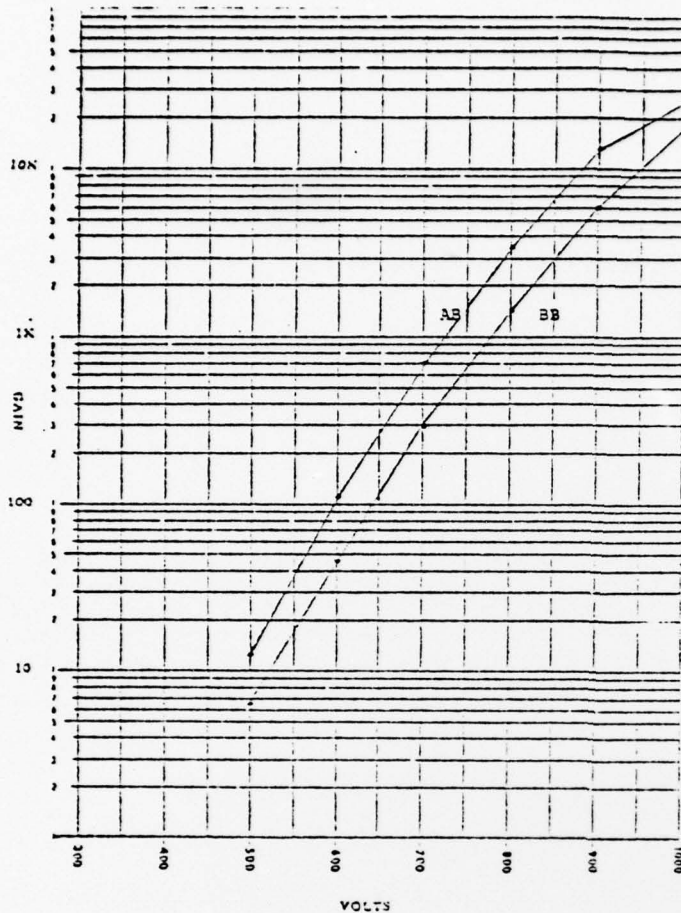


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Figure 13. TEST DATA SHEET  
MCP #542-26

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900 VOLTS MCP  
INPUT PENETRATION (VI)  $Al_2O_3$

VOLTS	OUTPUT CURRENT	GAIN
100	$2.4 \times 10^{-9}$	
200	$4.4 \times 10^{-9}$	
300	$7.2 \times 10^{-9}$	
400	$1.1 \times 10^{-8}$	
500	$1.5 \times 10^{-8}$	
600	$1.8 \times 10^{-8}$	
700	$2.0 \times 10^{-8}$	
800	$2.2 \times 10^{-8}$	
900	$2.3 \times 10^{-8}$	
1000	$2.33 \times 10^{-8}$	

7.0%

MCP S/N 464-T1  
VENDOR ITT  
DATE TESTED 2-22-77  
DIA. 0.975 inches  
THICKNESS 21.8 mils

CONDUCTIVITY: B. A. B. T. B.  
@ 500V 0.95 1.05 1.0  $\mu$  amps  
@ 1000V 2.1 2.3 2.1  $\mu$  amps  
INPUT:  $1.5 \times 10^{-12}$  AMPS/ $CM^2$

VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	$2.0 \times 10^{-10}$	6.7	
600	$1.4 \times 10^{-9}$	46	
700	$9.0 \times 10^{-9}$	300	
800	$4.6 \times 10^{-8}$	1533	
900	$1.9 \times 10^{-7}$	6333	
1000	$5.6 \times 10^{-7}$	18666	0

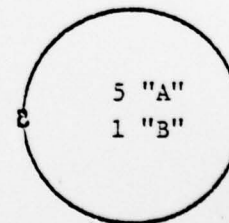
BEFORE  
IMAGE  
800 VEX

VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	$4.0 \times 10^{-10}$	13	
600	$3.5 \times 10^{-9}$	116	
700	$2.2 \times 10^{-8}$	733	
800	$1.05 \times 10^{-7}$	3500	
900	$4.3 \times 10^{-7}$	14322	
1000	$7.8 \times 10^{-7}$	26000	0

AFTER  
IMAGE  
800 VEX

VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	$1.7 \times 10^{-11}$	4.8	
600	$1.55 \times 10^{-10}$	45	
700	$1.05 \times 10^{-9}$	238	
800	$5.1 \times 10^{-9}$	1448	
900	$2.15 \times 10^{-8}$	6107	
1000	$7.0 \times 10^{-8}$	19880	0

TEST  
BENCH  
800 VEX



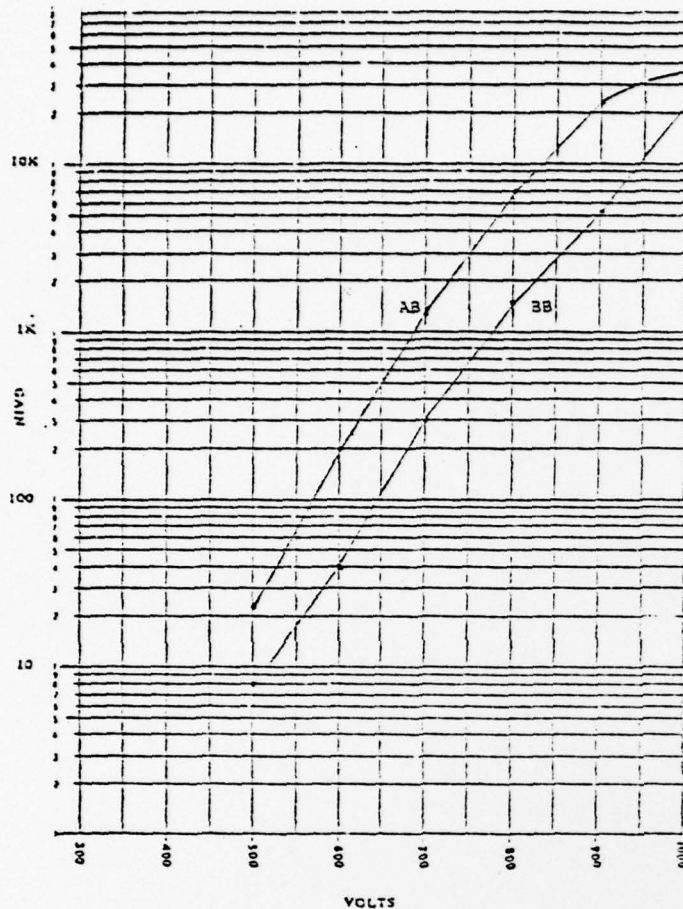
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Figure 14. TEST DATA SHEET  
MCP 464-T1

23  
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900 VOLTS MCP  
INPUT PENETRATION (Vi) AL<sub>2</sub>O<sub>3</sub>

VOLTS	OUTPUT CURRENT	GAIN
100E <sub>k</sub>	3.9 X 10 <sup>-9</sup>	
200	6.4 X 10 <sup>-9</sup>	
300	1.1 X 10 <sup>-9</sup>	
400	1.5 X 10 <sup>-8</sup>	
500	2.0 X 10 <sup>-8</sup>	
600	2.3 X 10 <sup>-8</sup>	
700	2.55 X 10 <sup>-8</sup>	
800	2.7 X 10 <sup>-8</sup>	
900	2.8 X 10 <sup>-8</sup>	
1000	2.9 X 10 <sup>-8</sup>	

7.0%

MCP S/N 464-T6  
VENDOR ITT  
DATE TESTED 2-15-77  
DIA. 0.975 inches  
THICKNESS 21.8 mils

CONDUCTIVITY: B.B. | A.B. | T.B.  
@ 500V 1.45 | 1.6 | 1.4 μ amps  
@ 1000V 3.1 | 3.4 | 3.0 μ amps  
INPUT: 1.5 x 10<sup>-12</sup> AMPS/CM<sup>2</sup>

MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	2.4 exp- 10	8.0	
600	1.2 exp- 9	40	
700	9.0 exp- 9	300	
800	5.0 exp- 8	1666	
900	1.6 exp- 7	5333	
1000	6.5 exp- 7	21666	0

BEFORE  
PAKE  
800 VEK

MCP

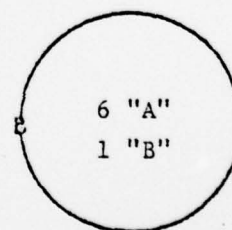
VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	7.0 exp- 10	23	
600	6.0 exp- 9	200	
700	4.1 exp- 8	1366	
800	2.1 exp- 7	1000	
900	7.1 exp- 7	23666	
1000	1.1 exp- 6	36660	0

AFTER  
PAKE  
800 VEK

MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	2.2 exp- 11	42	
600	1.9 exp- 10	36	
700	1.3 exp- 9	248	
800	6.4 exp- 9	1223	
900	2.7 exp- 8	5160	
1000	9.4 exp- 8	17970	0

TEST  
BENCH  
800 VEK



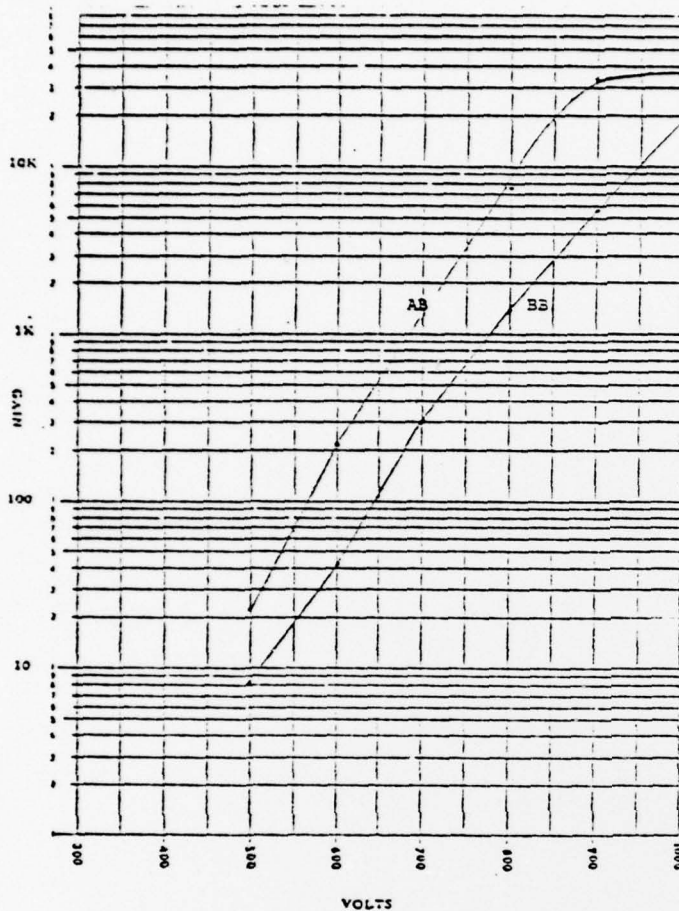
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Figure 15. TEST DATA SHEET  
MCP #464-T6

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900 VOLTS MCP  
INPUT PENETRATION (V) AL<sub>2</sub>O<sub>3</sub>

VOLTS	OUTPUT CURRENT	GAIN
100E <sub>k</sub>	4.5 x 10 <sup>-9</sup>	
200	9.0 x 10 <sup>-9</sup>	
300	1.6 x 10 <sup>-8</sup>	
400	2.4 x 10 <sup>-8</sup>	
500	3.2 x 10 <sup>-8</sup>	
600	3.9 x 10 <sup>-8</sup>	
700	4.4 x 10 <sup>-8</sup>	
800	4.7 x 10 <sup>-8</sup>	
900	5.0 x 10 <sup>-8</sup>	
1000	5.1 x 10 <sup>-8</sup>	

7.5%

MCP S/N 464-T5  
VENDOR ITT  
DATE TESTED 2-16-77  
DIA. 0.975 inches  
THICKNESS 21.8 mils

CONDUCTIVITY: B.B. | A.B. | T.B.  
@ 500V 1.2 | 1.3 | 1.15  $\mu$  cm<sup>2</sup>  
@ 1000V 2.7 | 2.85 | 2.4  $\mu$  cm<sup>2</sup>  
INPUT:  $1.5 \times 10^{-12}$  AMPS/CM<sup>2</sup>

MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	2.5 exp-10	8.3	
600	1.3 exp-9	43	
700	9.0 exp-9	300	
800	4.4 exp-8	1466	
900	1.7 exp-7	5666	
1000	5.7 exp-7	19000	0

BEFORE  
BAKE  
800 VEK

MCP

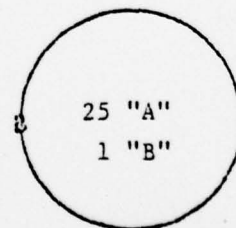
VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	7.0 exp-10	23	
600	6.6 exp-9	270	
700	4.4 exp-8	1466	
800	2.33 exp-7	7766	
900	7.4 exp-7	34666	
1000	1.1 exp-6	16666	0

AFTER  
BAKE  
800 VEK

MCP

VOLTS	OUTPUT CURRENT	GAIN	BKGD
500	3.6 exp-11	6.8	
600	3.3 exp-10	63	
700	2.2 exp-9	420	
800	1.2 exp-8	2766	
900	4.7 exp-8	3980	
1000	1.5 exp-7	28600	0

TEST  
BENCH  
800 VEK

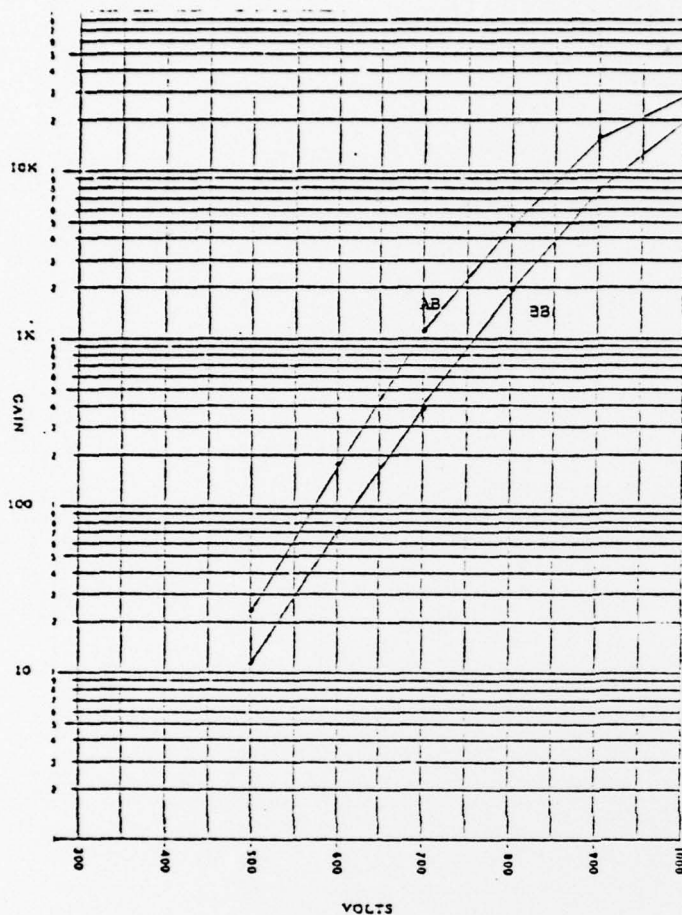


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Figure 16. TEST DATA SHEET  
MCP #464-T5

25  
UNCLASSIFIED

# UNCLASSIFIED



900 VOLTS MCP  
INPUT PENETRATION (V)  $Al_2O_3$

VOLTS	OUTPUT CURRENT	GAIN
100E <sub>k</sub>	$3.3 \times 10^{-9}$	
200	$6.0 \times 10^{-9}$	
300	$1.0 \times 10^{-8}$	
400	$1.7 \times 10^{-8}$	
500	$2.3 \times 10^{-8}$	
600	$3.0 \times 10^{-8}$	
700	$3.45 \times 10^{-8}$	
800	$3.85 \times 10^{-8}$	
900	$4.05 \times 10^{-8}$	
1000	$4.2 \times 10^{-8}$	

10%

MCP S/N 542-19  
VENDOR ITT  
DATE TESTED 2-28-77  
DIA. 0.975 inches  
THICKNESS 21.6 mils

CONDUCTIVITY: B.B. | A.P. | T.P.  
@ 500V 1.3 | 1.35 | 1.3  $\mu$  amps  
@ 1000V 2.85 | 2.95 | 2.7  $\mu$  amps  
INPUT:  $1.5 \times 10^{-12}$  AMPS/CM<sup>2</sup>

MCP VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	$4.0 \times 10^{-10}$	12	
600	$2.3 \times 10^{-9}$	69	
700	$1.3 \times 10^{-8}$	390	
800	$6.5 \times 10^{-8}$	1969	
900	$2.5 \times 10^{-7}$	7575	
1000	$6.6 \times 10^{-7}$	20000	0

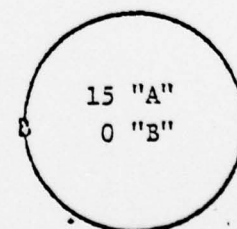
BEFORE  
PAKE  
800 VEK

MCP VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	$8.0 \times 10^{-10}$	24	
600	$5.8 \times 10^{-9}$	175	
700	$3.7 \times 10^{-8}$	1121	
800	$1.6 \times 10^{-7}$	4848	
900	$5.7 \times 10^{-7}$	17270	
1000	$9.0 \times 10^{-7}$	27272	0

AFTER  
PAKE  
800 VEK

MCP VOLTS	OUTPUT CURRENT	GAIN	BKGD.
500	$3.8 \times 10^{-11}$	7.2	
600	$3.2 \times 10^{-10}$	61	
700	$2.0 \times 10^{-9}$	382	
800	$9.3 \times 10^{-9}$	1776	
900	$3.7 \times 10^{-8}$	7070	
1000	$1.1 \times 10^{-7}$	21000	0

TEST  
BENCH  
800 VEK

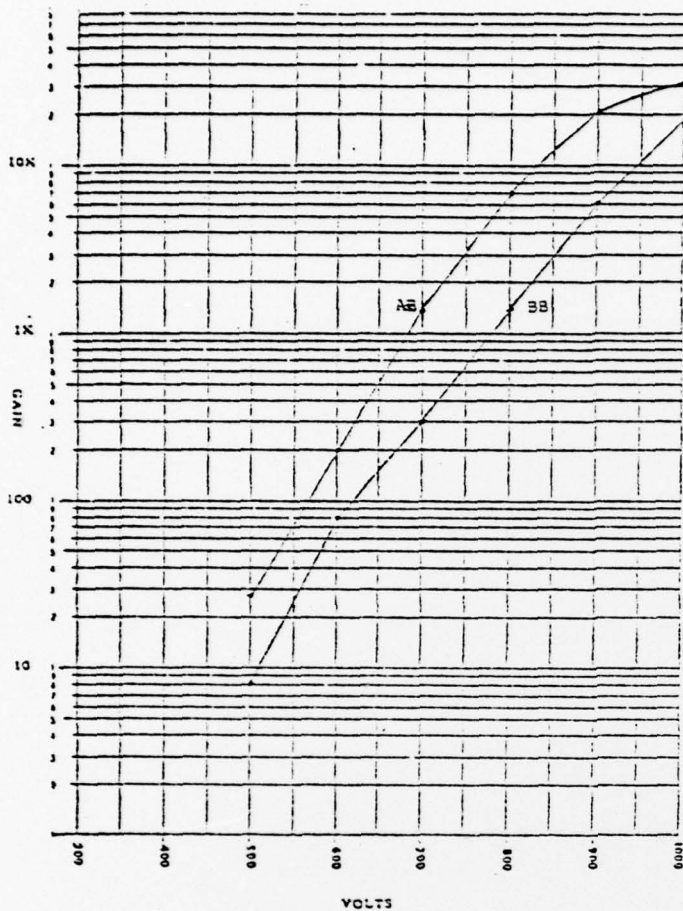


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Figure 17. TEST DATA SHEET  
MCP #542-19

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MCP S/N 542-29  
 VENDOR ITT  
 DATE TESTED 3-3-77  
 DIA. 0.975 inches  
 THICKNESS 21.6 mils

CONDUCTIVITY: E.B. | A.B. | T.B.  
 @ 500V 1.15 | 1.2 | 1.2  $\mu$  amps  
 @ 1000V 2.53 | 2.65 | 2.4  $\mu$  amps  
 INPUT:  $1.5 \times 10^{-12}$  AMPS/CM<sup>2</sup>

MCP				
VOLTS	OUTPUT CURRENT	GAIN	BKGD.	
500	2.5 exp-10	8.3		BEFORE BAKE 800 VEK
600	2.4 exp-9	80		
700	9.0 exp-9	300		
800	4.7 exp-8	1566		
900	1.2 exp-7	6333		
1000	5.6 exp-7	18666	0	

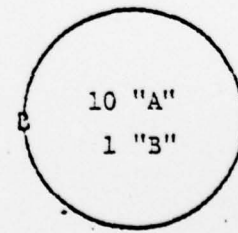
MCP				
VOLTS	OUTPUT CURRENT	GAIN	BKGD.	
500	8.5 exp-10	28		AFTER LAKE 800 VEK
600	6.0 exp-9	200		
700	4.3 exp-8	1433		
800	2.1 exp-7	7000		
900	6.5 exp-7	21666		
1000	9.5 exp-7	31666	0	

MCP				
VOLTS	OUTPUT CURRENT	GAIN	BKGD.	
500	6.8 exp-11	13		TEST BENCH 800 VEK
600	5.9 exp-10	111		
700	3.7 exp-9	707		
800	1.9 exp-8	3630		
900	7.0 exp-8	13400		
1000	2.1 exp-7	40100	0	

900 VOLTS MCP  
 INPUT PENETRATION (VI) AL<sub>2</sub>O<sub>3</sub>

VOLTS	OUTPUT CURRENT	GAIN
100 Ek	6.5 X10 <sup>-9</sup>	
200	1.3 X10 <sup>-8</sup>	
300	2.3 X10 <sup>-8</sup>	
400	3.6 X10 <sup>-8</sup>	
500	5.2 X10 <sup>-8</sup>	
600	6.5 X10 <sup>-8</sup>	
700	7.6 X10 <sup>-8</sup>	
800	8.4 X10 <sup>-8</sup>	
900	8.9 X10 <sup>-8</sup>	
1000	9.3 X10 <sup>-8</sup>	

10%



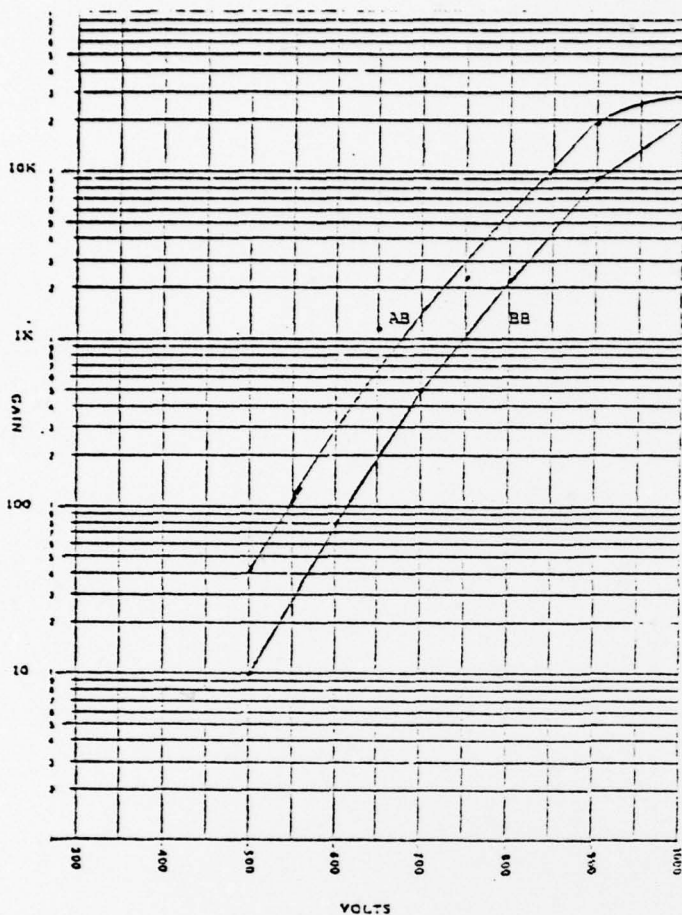
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Figure 18. TEST DATA SHEET  
 MCP #542-29

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900 VOLTS MCP  
INPUT PENETRATION (V):  $Al_2O_3$

VOLTS	OUTPUT CURRENT	GAIN
100 $E_k$	$5.4 \times 10^{-9}$	
200	$1.1 \times 10^{-8}$	
300	$1.3 \times 10^{-8}$	
400	$2.6 \times 10^{-8}$	
500	$3.4 \times 10^{-8}$	
600	$4.1 \times 10^{-8}$	
700	$4.6 \times 10^{-8}$	
800	$4.9 \times 10^{-8}$	
900	$5.12 \times 10^{-8}$	
1000	$5.25 \times 10^{-8}$	

8%

MCP S/N 508-20  
VENDOR ITT  
DATE TESTED 2-17-77  
DIA. 0.975 inches  
THICKNESS 22.2 mils

CONDUCTIVITY: B. | A.B. | T.B.  
@ 500V 0.9 | 0.9 | 10.9  $\mu$  amps  
@ 1000V 1.95 | 2.05 | 2.8  $\mu$  amps  
INPUT:  $1.5 \times 10^{-12}$  AMPS/CM<sup>2</sup>

MCP	VOLTS	OUTPUT CURRENT	GAIN	BKGD.
	500	3.0 exp- 10	10	
	600	2.4 exp- 9	30	
	700	1.5 exp- 8	500	
	800	7.1 exp- 8	2366	
	900	2.67 exp- 7	8900	
	1000	6.1 exp- 7	20133	0

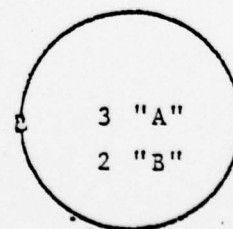
BEFORE  
BAKE  
800 VEK

MCP	VOLTS	OUTPUT CURRENT	GAIN	BKGD.
	500	1.3 exp- 9	43	
	600	3.6 exp- 8	1200	
	700	7.0 exp- 8	2233	
	800	3.0 exp- 7	10000	
	900	5.8 exp- 7	19330	
	1000	8.3 exp- 7	27666	0

AFTER  
BAKE  
800 VEK

MCP	VOLTS	OUTPUT CURRENT	GAIN	BKGD.
	500	5.7 exp- 11	11	
	600	5.0 exp- 10	96	
	700	3.2 exp- 9	610	
	800	1.6 exp- 8	2050	
	900	6.0 exp- 8	1500	
	1000	1.6 exp- 7	20500	0

TEST  
BENCH  
800 VEK



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Figure 19. TEST DATA SHEET  
MCP #508-20

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flood gun testing capability to simulate tube test conditions.

## 3.0 CONCLUSIONS (U)

- (U) Careful picking and cleaning of MCP's prior to lacquering and the addition of an edge grind to remove polishing compound have resulted in a cleaner MCP and hence, in a reduction of type A and B holes. It was also established that the application of a thicker lacquer film further reduced the number of type A and B holes. Higher quality ion barrier films can now be produced at high yield by utilizing the oil-free Varian evaporator and a dual shutter system to precisely control deposition rate and film thickness.
- (U) Smooth MCP surfaces have been achieved with the introduction of a prepolish technique which eliminates scratches. Because of difficulties encountered in reproducing uniform fire polished surfaces, the fire polish technique was discontinued in favor of the pre-polish technique.
- (U) Evaluation of  $Al_2O_3$  filmed MCP's in the demountable test head and in tubes, has indicated that film quality evaluation is strongly dependent on test technique employed. To increase test reliability and to achieve better correlation with evaluation in tubes, both the engineering demountable test head and the newly constructed bakeable and demountable system will be equipped with a flood gun arrangement.

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## 4.0 SCHEDULE (U)

Effort planned for the next quarter include:

- 4.1 Complete debugging of Bakeable Demountable Test System. (U)
- 4.2 Fabricate and Test Five (5) Engineering Samples to Category III Requirements. (U)
- 4.3 Install Flood Gun Viewing Device for  $\text{Al}_2\text{O}_3$  MCP Evaluation in both Demountable Systems. (U)
- 4.4 Continue investigation of defects and elimination of defects by using thick  $\text{Al}_2\text{O}_3$  filmed MCP's. (U)
- 4.5 Complete MCP Surface Improvement by Utilizing Prepolish Technique. (U)

## 5.0 CONFERENCES AND REPORTS (U)

### 5.1 Conferences (U)

(U) Mr. John Rennie visited ITT EOPD on March 10th and 11th and reviewed progress to date and planning for 4th quarter.

### 5.2 Reports (U)

(U) The draft copy of the second quarterly report has been submitted. Monthly progress letters for January, February, and March have been submitted.

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## 6.0 GLOSSARY (U)

- $\text{\AA}$  - Angstrom
- $\text{Al}_2\text{O}_3$  - Chemical abbreviation for aluminum oxide
- Lacquer - An organic liquid which is applied to the MCP to temporarily cover the channel holes. After a smooth sheet of  $\text{Al}_2\text{O}_3$  is evaporated on top of the lacquer, the lacquer is removed by baking in oxygen.
- MCP - Microchannel plate

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